

Ferromagnetic Resonance in Coupled Magnetic Multilayer Systems

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Received October 19, 1992

Ferromagnetic resonance provides a unique technique to evaluate the strength of interlayer exchange coupling between ferromagnetic layers separated by "non-magnetic" layers in magnetic multilayer structures as well as the internal magnetic energies within each magnetic layer. The dispersion relations, which are sensitive to both the effective uniaxial anisotropy energy and the interlayer exchange coupling constant A_{12} , have been calculated for systems consisting of two identical ferromagnetic layers either parallel or anti-parallel coupled through a "non-magnetic" spacer. The extensions of these calculations to asymmetric structures and/or multilayer structures are discussed. Ferromagnetic resonance techniques have been applied to many magnetic multilayer structures and several results will be reviewed.

I. Introduction

Multilayered structures constructed by alternating layers of ferromagnetic materials, such as Co, Fe, Ni and Permalloy, and separated by nominally "non-magnetic" materials have received much attention in the past several years. These nominally "non-magnetic" materials include the noble metals, Ag, Au and Cu, and in addition non-ferromagnetic materials such as Pt, Pd, Cr, and Ru. Recent advances in sample preparation techniques, such as molecular beam epitaxial methods (MBE) have made it possible to produce a large variety of magnetic layered structures with repeatable magnetic properties. The interest has been concentrated on the novel magnetic behaviors which have only been observed for films with layer thicknesses on the order of several atomic layers, as well as the possibility of fabricating new materials for practical applications. In the early work on a Fe/Cr structure^{1,2}, a clear-cut anti-parallel coupling between the adjacent Fe layers was observed. Further investigations on the same structure revealed an oscillation behavior between parallel and anti-parallel coupling as a function of the Cr thickness³. For the application interest, this series also exhibits a giant magnetoresistance due to the change in the conduction electron scattering mechanisms as the orientation of the magnetization is modified by the application of an external magnetic field⁴. In the Co/Pt or Co/Pd multilayer structures^{5,6}, the internal uniaxial anisotropy energy was significantly enhanced with the decrease of the Co thickness. Samples with perpendicular magnetic anisotropy were reported as the Co thickness was reduced below $\sim 15 \text{ \AA}$. Another important property of

this series was the enhancement of the magneto-Kerr effect at shorter wave-length which increased the interest on Co/Pt and Co/Pd multilayer structures as a prominent perpendicular magneto-optical recording media.

In each case, these unusual characteristics are due to a significant modification of the internal energies of the magnetic multilayer structures, especially the uniaxial anisotropy energy developed from the interface between the magnetic/"non-magnetic" layer and the interlayer exchange energy between two adjacent ferromagnetic layers through "non-magnetic" spacers. As will be shown in this paper, magnetic resonance is a useful technique to investigate these magnetic properties. In the ferromagnetic resonance (FMR) experiment, the position of the uniform precessing resonance mode is sensitive to the magnetic anisotropy energy, the magnetostatic energy and the Zeeman energy. The variation of the uniform mode as a function of the orientation of the applied field can, in general, separate the contributions from different energy terms. In addition to the uniform mode, there are high order spin-wave modes corresponding to the rf magnetization having either an amplitude or a phase difference from one magnetic layer to the next. Since an extra exchange energy term is involved in the internal energies, the shift of the spin-wave modes from the uniform mode will provide an evaluation of the interlayer exchange coupling strength.

In section II, the theory of the coupled ferromagnetic film resonance (CFFR) will be introduced. As a special example, the theory will be applied to a system consisting of two identical ferromagnetic layers separated by a "non-magnetic" layer. The parallel and anti-

parallel interlayer exchange coupling will be considered separately with the applied external field along both the parallel and normal orientations to the film plane.

In section III, some experimental results of the multilayer structures will be discussed. Since the range of variables that can be chosen for a given structure is very broad and each structure will have its own unique set of material parameter, it is difficult to "catalog" all the data available from the various magnetic resonance experiments.

A technique that obtains complimentary information to CFFR is Brillouin light scattering in which an incoming light wave scatters off the structure and excites or absorbs the same magnetic excitations as observed in the magnetic resonance process. Instead of sweeping the magnetic field at a constant frequency in CFFR, the resonance condition is achieved by "sweeping" frequencies at constant applied field in Brillouin light scattering experiment. Details about the experimental set-up and results were given in the literatures^{1,2,7-12}.

II. Resonance Condition

II.1. General Consideration

When a ferromagnetic material is placed in an applied static magnetic field, the magnetic moments in the material, if perturbed from their equilibrium orientation, will precess around their equilibrium direction due to the torque which can be expressed in terms of either an effective internal field \mathbf{H}_{eff} or a gradient of the expression for the energy density, \mathcal{E} , such that,

$$\frac{1}{\gamma} \frac{d\mathbf{M}}{dt} = -\mathbf{M} \times \mathbf{H}_{eff} = \mathbf{M} \times \nabla_{\mathbf{M}} \mathcal{E}, \quad (1)$$

where γ is the gyromagnetic ratio and \mathbf{M} is the magnetization. The equation of motion can be solved by using the coordinate system shown in Figure 1 in which the small deviations from equilibrium are in the \hat{e}_θ and \hat{e}_ϕ directions. This orientation of the coordinate system is used in order that the dispersion relation can be obtained as a function of the orientation of \mathbf{M} from a direction normal to the film to one lying in the film plane. In this coordinate system the magnetization has the form

$$\mathbf{M} = M_0 \hat{e}_z + m_\theta \hat{e}_\theta + m_\phi \hat{e}_\phi, \quad (2)$$

where m_θ and m_ϕ are the small transverse components of the magnetization associated with the precession, $m_\theta = M \delta\theta$, $m_\phi = M \sin\theta \delta\phi$ and $\delta\theta$ and $\delta\phi$ are small deviations from the equilibrium direction.

In the system with N ferromagnetic layers separated by "non-magnetic" layers but coupled by an exchange interaction, it is convenient to use the energy per film area E instead of volume energy density \mathcal{E} :

$$E = \sum_{i=1}^N t_i \mathcal{E}_i - \sum_{i=1}^{N-1} A_{i,i+1} \frac{\mathbf{M}_i \cdot \mathbf{M}_{i+1}}{M_i M_{i+1}}, \quad (3)$$

where t_i and \mathcal{E}_i are the thickness and energy density of the i th layer, and $A_{i,i+1}$ is the exchange energy per unit surface area between the i th and $(i+1)$ th layers. The negative sign is chosen so that $A_{i,i+1}$ will be positive for parallel coupled system and negative for anti-parallel system.

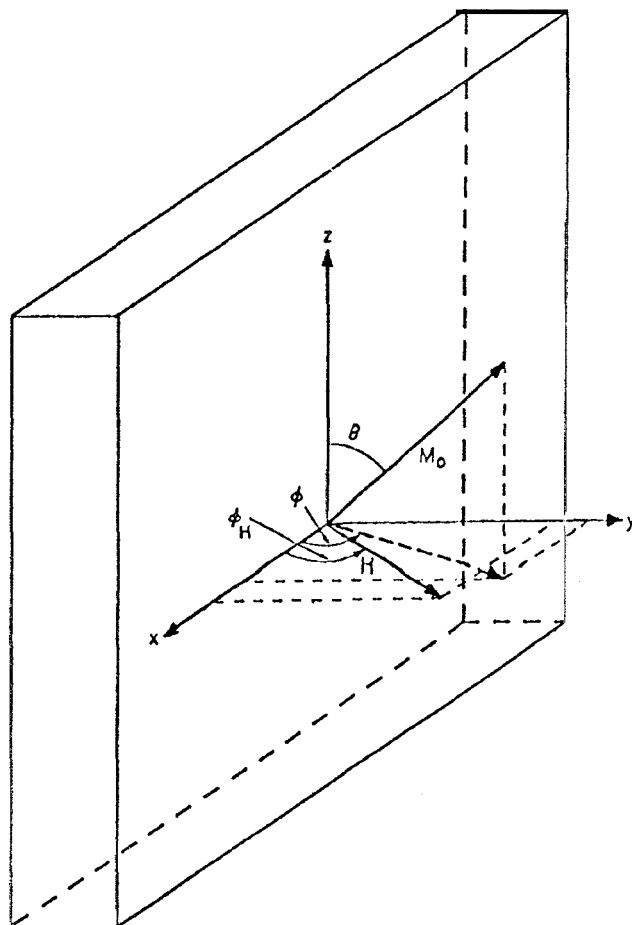


Figure 1: The coordinate system used for the evaluation of the CFFR condition.

The resonance equation (1) will have the new form:

$$\frac{1}{\gamma_i} \frac{d\mathbf{M}_i}{dt} = \mathbf{M}_i \times \left(\frac{1}{t_i} \nabla_{\mathbf{M}_i} E \right), \quad (i = 1, 2, \dots, N). \quad (4)$$

In the equilibrium orientation, the magnetization will not have a variation in either time or space across each magnetic layer and Eq. (4) reduces to

$$\mathbf{M}_i \times \frac{1}{t_i} \nabla_{\mathbf{M}_i} E = \frac{1}{t_i} \left(E_{\theta_i} \hat{e}_\theta - \frac{E_{\phi_i}}{\sin\theta_i} \hat{e}_\phi \right) = 0, \quad (5)$$

where the notation $E_{\theta_i} = \partial E / \partial \theta_i$ and $E_{\phi_i} = \partial E / \partial \phi_i$ is used.

The equations of motion are linearized by expanding Eq. (4) about the equilibrium orientation and retaining only terms to the first order of m_{θ_i} and m_{ϕ_i} expressed in Eq. (2). In linearized form the equations of motion become a set of $2N$ equations:

$$\begin{aligned}
 \frac{1}{\gamma_1} \frac{d}{dt} m_{\theta_1} &= -\frac{1}{t_1 M_1 \sin \theta_1} \left(E_{\theta_1 \phi_1} m_{\theta_1} + \frac{E_{\phi_1 \phi_1}}{\sin \theta_1} m_{\phi_1} \right) - \frac{1}{t_1 M_2 \sin \theta_1} \left(E_{\theta_2 \phi_1} m_{\theta_2} + \frac{E_{\phi_1 \phi_2}}{\sin \theta_2} m_{\phi_2} \right), \\
 \frac{1}{\gamma_1} \frac{d}{dt} m_{\phi_1} &= \frac{1}{t_1 M_1} \left(E_{\theta_1 \theta_1} m_{\theta_1} + \frac{E_{\theta_1 \phi_1}}{\sin \theta_1} m_{\phi_1} \right) + \frac{1}{t_1 M_2} \left(E_{\theta_1 \theta_2} m_{\theta_2} + \frac{E_{\theta_1 \phi_2}}{\sin \theta_2} m_{\phi_2} \right), \\
 \frac{1}{\gamma_i} \frac{d}{dt} m_{\theta_i} &= -\frac{1}{t_i M_i \sin \theta_i} \left(E_{\theta_i \phi_i} m_{\theta_i} + \frac{E_{\phi_i \phi_i}}{\sin \theta_i} m_{\phi_i} \right) - \frac{1}{t_i M_{i+1} \sin \theta_i} \left(E_{\theta_{i+1} \phi_i} m_{\theta_{i+1}} + \frac{E_{\phi_i \phi_{i+1}}}{\sin \theta_{i+1}} m_{\phi_{i+1}} \right) \\
 &\quad - \frac{1}{t_i M_{i-1} \sin \theta_i} \left(E_{\theta_{i-1} \phi_i} m_{\theta_{i-1}} + \frac{E_{\phi_{i-1} \phi_i}}{\sin \theta_{i-1}} m_{\phi_{i-1}} \right) \quad (i = 2, \dots, N-1), \\
 \frac{1}{\gamma_i} \frac{d}{dt} m_{\phi_i} &= \frac{1}{t_i M_i} \left(E_{\theta_i \theta_i} m_{\theta_i} + \frac{E_{\theta_i \phi_i}}{\sin \theta_i} m_{\phi_i} \right) + \frac{1}{t_i M_{i+1}} \left(E_{\theta_i \theta_{i+1}} m_{\theta_{i+1}} + \frac{E_{\theta_i \phi_{i+1}}}{\sin \theta_{i+1}} m_{\phi_{i+1}} \right) \\
 &\quad + \frac{1}{t_i M_{i-1}} \left(E_{\theta_{i-1} \theta_i} m_{\theta_{i-1}} + \frac{E_{\theta_i \phi_{i-1}}}{\sin \theta_{i-1}} m_{\phi_{i-1}} \right) \quad (i = 2, \dots, N-1), \\
 \frac{1}{\gamma_N} \frac{d}{dt} m_{\theta_N} &= -\frac{1}{t_N M_N \sin \theta_N} \left(E_{\theta_N \phi_N} m_{\theta_N} + \frac{E_{\phi_N \phi_N}}{\sin \theta_N} m_{\phi_N} \right) - \\
 &\quad \frac{1}{t_N M_{N-1} \sin \theta_N} \left(E_{\theta_{N-1} \phi_N} m_{\theta_{N-1}} + \frac{E_{\phi_{N-1} \phi_N}}{\sin \theta_{N-1}} m_{\phi_{N-1}} \right), \\
 \frac{1}{\gamma_N} \frac{d}{dt} m_{\phi_N} &= \frac{1}{t_N M_N} \left(E_{\theta_N \theta_N} m_{\theta_N} + \frac{E_{\theta_N \phi_N}}{\sin \theta_N} m_{\phi_N} \right) + \\
 &\quad \frac{1}{t_N M_{N-1}} \left(E_{\theta_{N-1} \theta_N} m_{\theta_{N-1}} + \frac{E_{\theta_N \phi_{N-1}}}{\sin \theta_{N-1}} m_{\phi_{N-1}} \right), \tag{6}
 \end{aligned}$$

where $E_{\theta_i \theta_j} = \partial^2 E / \partial \theta_i \partial \theta_j$, $E_{\phi_i \phi_j} = \partial^2 E / \partial \phi_i \partial \phi_j$ and $E_{\theta_i \phi_j} = \partial^2 E / \partial \theta_i \partial \phi_j$.

Eq. (6) can be expressed in matrix form^{13,14} with the roots of the determinant giving the resonance frequencies of the multilayer system. In general N modes at different frequencies will be obtained for a given applied field. In the case that the N magnetic layers are identical and not coupled with their adjacent layers, those N modes will be degenerate and the dispersion relation will be the same as that of a single magnetic layer system. The ellipticity of the precession, $m_{\theta_i} / m_{\phi_i}$, and, in the case of coupled layers, the phase shift from one layer to another can also be obtained from the eigenvector $(m_{\theta_1}, m_{\phi_1}, \dots, m_{\theta_N}, m_{\phi_N})$ corresponding to each mode.

The internal energies \mathcal{E}_i that normally contribute to the resonance equations (6) are the following:

a. Zeeman Energy

In the presence of an applied magnetic field \mathbf{H}_0 , the energy expression is given as

$$\begin{aligned}
 \mathcal{E}_i^z &= -\mathbf{H}_0 \cdot \mathbf{M}_i = -H_0 M_i [\cos \theta_H \cos \theta_i \\
 &\quad + \sin \theta_H \sin \theta_i \cos(\phi_i - \phi_H)], \tag{7}
 \end{aligned}$$

where θ_H and ϕ_H are the orientation angles of the applied external field \mathbf{H}_0 .

b. Cubic Crystalline Anisotropy Energy

In this contribution the crystalline anisotropy energy will be considered for the condition that all three unique axes in the cubic structure may be oriented normal to the film, [001], [110] and [111]. For a [001] oriented film the energy expression has the form

$$\begin{aligned}
 \mathcal{E}_{[001],i}^c &= \frac{K_{1,i}}{M_i^4} (M_{x,i}^2 M_{y,i}^2 + M_{y,i}^2 M_{z,i}^2 + M_{z,i}^2 M_{x,i}^2) \\
 &\quad + \frac{K_{2,i}}{M_i^6} M_{x,i}^2 M_{y,i}^2 M_{z,i}^2 \\
 &= K_{1,i} \left(\frac{\sin^4 \theta_i \sin^2 2\phi_i}{4} + \frac{\sin^2 2\theta_i}{4} \right) \\
 &\quad + K_{2,i} \frac{\sin^2 \theta_i \sin^2 2\theta_i \sin^2 2\phi_i}{16}. \tag{8}
 \end{aligned}$$

For a [110] oriented film the energy expression has the form (x || [001])

$$\begin{aligned}
\mathcal{E}_{[110],i}^c &= \frac{K_{1,i}}{M_i^4} \left(M_{x,i}^2 M_{y,i}^2 + M_{x,i}^2 M_{z,i}^2 + \frac{M_{y,i}^4}{4} + \frac{M_{z,i}^4}{4} - \frac{M_{y,i}^2 M_{z,i}^2}{2} \right) \\
&+ \frac{K_{2,i}}{M_i^6} \left(\frac{M_{x,i}^2 M_{y,i}^4}{4} + \frac{M_{x,i}^2 M_{z,i}^4}{4} - \frac{M_{x,i}^2 M_{y,i}^2 M_{z,i}^2}{2} \right) \\
&= K_{1,i} \left(\frac{\sin^4 \theta_i \sin^2 2\phi_i}{4} + \frac{\sin^2 \theta_i \cos^2 \phi_i}{4} + \frac{\sin^4 \theta_i \sin^4 \phi_i}{4} + \frac{\cos^4 \theta_i}{4} - \frac{\sin^2 2\theta_i \sin^2 \phi_i}{8} \right) \\
&+ K_{2,i} \left(\frac{\sin^6 \theta_i \sin^2 \phi_i \sin^2 2\phi_i}{16} + \frac{\sin^2 2\theta_i \cos^2 \theta_i \cos^2 \phi_i}{16} - \frac{\sin^2 \theta_i \sin^2 2\theta_i \sin^2 2\phi_i}{32} \right). \quad (9)
\end{aligned}$$

For a [111] oriented film the energy expression has the form (x || [112])

$$\begin{aligned}
\mathcal{E}_{[111],i}^c &= \frac{K_{1,i}}{M_i^4} \left(\frac{M_{x,i}^4}{4} + \frac{M_{y,i}^4}{3} + \frac{M_{z,i}^4}{4} + \frac{M_{x,i}^2 M_{z,i}^2}{2} + \frac{\sqrt{2}}{3} M_{x,i}^3 M_{y,i} - \sqrt{2} M_{x,i} M_{y,i} M_{z,i}^2 \right) \\
&+ \frac{K_{2,i}}{M_i^6} \frac{(\sqrt{2} M_{x,i} - M_{y,i})^2 [(M_{x,i} + \sqrt{2} M_{y,i})^2 - 3 M_{z,i}^2]^2}{108} \\
&= K_{1,i} \left(\frac{\sin^4 \theta_i \cos^4 \phi_i}{4} + \frac{\sin^4 \theta_i \sin^4 \phi_i}{3} + \frac{\cos^4 \theta_i}{4} + \frac{\sin^2 2\theta_i \cos^2 \phi_i}{8} \right) \\
&+ \frac{\sqrt{2}}{3} \sin^4 \theta_i \sin \phi_i \cos^3 \phi_i - \frac{\sqrt{2}}{8} \sin^2 2\theta_i \sin 2\phi_i \\
&+ K_{2,i} \frac{\sin^2 \theta_i (\sqrt{2} \cos \phi_i - \sin \phi_i)^2 [\sin^2 \theta_i (\cos \phi_i + \sqrt{2} \sin \phi_i)^2 - 3 \cos^2 \theta_i]^2}{108}. \quad (10)
\end{aligned}$$

c. Uniaxial anisotropy energy

In addition to the demagnetization energy producing an easy plane material, a uniaxial anisotropy energy can be introduced into the material if it has hexagonal symmetry with the c-axis normal to the plane or if an

induced uniaxial anisotropy energy is present due to strains developed during growth or in the case of alloy films, a regular variation in the position of certain ions in the lattice producing a growth induced anisotropy energy. To the fourth order of $M_{y,i}$ the form for the energy expression will be;

$$\mathcal{E}_{u,i} = -K_{2u,i}^{eff} \frac{M_{y,i}^2}{M_i^2} - K_{4u,i} \frac{M_{y,i}^4}{M_i^4} = -K_{2u,i}^{eff} \sin^2 \theta_i \sin^2 \phi_i - K_{4u,i} \sin^4 \theta_i \sin^4 \phi_i. \quad (11)$$

The first term in Eq. (11) will include the demagnetization energy $2\pi M_{y,i}^2$ and the internal uniaxial anisotropy energy $-K_{2u,i} M_{y,i}^2 / M_i^2$ following the relation;

$$K_{2u,i}^{eff} = K_{2u,i} - 2\pi M_i^2. \quad (12)$$

d. Surface anisotropy energy

One of the important contributions to the uniaxial anisotropy energy $K_{2u,i}$ comes from the surface anisotropy^{5,15-19}. In the case where a magnetic layer has a thickness greater than the magnetic correlation length, which is on the order of a few hundred Angstroms, the presence of a surface anisotropy energy,

K_{sur} , will influence the resonance condition of the surface spins and produce a "pinned" boundary condition that gives rise to standing spin-wave modes that can be excited across the thickness of the film¹³. In the case of typical multilayer films, the film thicknesses are on the order of 10 \AA and the excitation energy of the higher order spin-waves associated with a single layer would be so large, on the order of 10^2 tesla, that they will not be observed in the CFFR experiment. As a result the surface anisotropy energy, instead of affecting only the surface of each film, will be weighted over the film thickness to produce an effective volume anisotropy energy having the form

$$K_{2u,i} = K_{2u,i}^b + 2K_{sur,i}/t_i, \quad (13)$$

where $K_{2u,i}^b$ is the bulk uniaxial anisotropy energy and the factor of 2 in the second term arises from the two surfaces acting on each layer.

Another contribution to the energy density \mathcal{E}_i comes from the direct exchange interaction between magnetic spins within each layer. However, as will be shown later, the strength of the exchange interaction between two magnetic layers, A_{12} , is much smaller ($10^{-3} \sim 10^{-2}$) than that within the ferromagnetic layer itself. As a result in the normal CFFR modes, the rf magnetization vectors in each individual ferromagnetic layers are nearly uniform across the film but they can have both a phase and an amplitude difference from one ferromagnetic layer to the next¹⁸. As a result, to first order each layer is treated as a continuous media with a uniform magnetization \mathbf{M}_i . In some multilayer system for which the magnetic layer thickness is on the order of $100 \sim 1000 \text{ \AA}$, the contribution from the exchange interaction within each layer may not be negligible. In this case the calculations must include the spin-wave energy within each layer as reported in the literature^{11,12,20-22}.

c. In-plane anisotropy energy

In the case of the anti-parallel coupled films, an in-plane uniaxial anisotropy energy, in addition to that having a unique direction normal to the structure, will produce a unique axis in the plane of the film. Two orientations of the applied magnetic field will be of interest for our purpose. One will be with the easy axis parallel to the x-axis and the form of the energy expression will be

$$\mathcal{E}_{D,i}^x = -D_i^x M_{z,i}^2 / M_i^2 = -D_i^x \sin^2 \theta_i \cos^2 \phi_i \quad (14)$$

and the other will be with the easy axis parallel to z-axis and the form will be

$$\mathcal{E}_{D,i}^z = -D_i^z M_{z,i}^2 / M_i^2 = -D_i^z \cos^2 \theta_i, \quad (15)$$

where D_i^x and D_i^z are the in-plane anisotropy energy constants for which the easy axis is along the x-axis or the z-axis respectively when the D values are positive.

f. Linewidth and damping parameters

The linewidth in the CFFR spectrum is relatively broader than that of a single ferromagnetic film. One of the most important contribution to the linewidth may be due to the inhomogeneities in the internal fields of the sample²³. These inhomogeneities may arise from non-homogeneous stresses in the film or any variation in the layer thickness from layer to layer or the fluctuation of the interlayer diffusion between the ferromagnetic and "non-magnetic" layers.

Another contribution, when the inhomogeneities do not dominate, is the spin relaxation processes in the multilayer films. Relaxation terms cannot be included directly into the energy expression and must be added to the right hand side of the equations of motion, Eq.(4), as a phenomenological damping term. The damping term in the Gilbert form is

$$-\frac{\alpha}{\gamma_i M_i} \mathbf{M}_i \times \frac{d}{dt} \mathbf{M}_i, \quad (16)$$

where α is the damping parameter. This phenomenological term predicts a symmetric Lorentz shape absorption line with the linewidth $\Delta H = 2\omega\alpha/\gamma_i$ if the i th layer is not coupled with the other layers¹⁴.

The intensity of the CFFR modes is sensitive to both the amplitude and the phase variation from one layer to another. In the microwave resonance, the rf pumping field has a space variation, on the order of 1 cm, much larger than the sample's dimension which is on the order of 1 mm. As a result the rf field across the film surface can be treated as a uniform field which only varies as a function of time. Assuming that the direction of the rf field is always parallel to the z direction and \mathbf{M}_i stays in the x-y plane (i.e. $\theta_i = \pi/2$) the intensity of each mode will have the relation^{14,24}

$$I \propto \left(\sum_{i=1}^N t_i m_{\theta,i} \right)^2 / \sum_{i=1}^N t_i (m_{\theta,i}^2 + m_{\phi,i}^2). \quad (17)$$

In the next part, a ferromagnetically coupled ($A_{i,j} > 0$) trilayer system, which includes two ferromagnetic layers separated by a "non-magnetic" layer, will be considered.

II.2. Parallel Coupled Trilayer System

In the trilayer system, the internal energy density for each layer, \mathcal{E}_1 and \mathcal{E}_2 may include any of the energy terms in Eq. (7) through Eq. (15). As observed in the previous section, the details of the internal energies have a profound effect on the positions of the resonance. However, for the purpose of illustration in this section, the forms of the energy to be used in the analysis will be limited to the Zeeman energy with the external field \mathbf{H}_0 in the x-y plane, the effective uniaxial

anisotropy energy leaving a unique direction normal to the plane (y-axis) and the interlayer exchange energy. The calculation including the cubic anisotropy energy

can be found in the literature^{12,23,25}. The energy per unit area will then have the form:

$$\begin{aligned}
 E &= -\mathbf{H}_0 \cdot (t_1 \mathbf{M}_1 + t_2 \mathbf{M}_2) - \left(t_1 K_{2u,i}^{eff} \frac{M_{y,1}^2}{M_1^2} + t_2 K_{2u,i}^{eff} \frac{M_{y,2}^2}{M_2^2} \right) - A_{12} \frac{\mathbf{M}_1 \cdot \mathbf{M}_2}{M_1 M_2} \\
 &= -H_0 [t_1 M_1 \sin \theta_1 \cos(\phi_1 - \phi_H) + t_2 M_2 \sin \theta_2 \cos(\phi_2 - \phi_H)] - t_1 K_{2u,1}^{eff} \sin^2 \theta_1 \sin^2 \phi_1 \\
 &\quad - t_2 K_{2u,2}^{eff} \sin^2 \theta_2 \sin^2 \phi_2 - A_{12} [\cos \theta_1 \cos \theta_2 + \sin \theta_1 \sin \theta_2 \cos(\phi_1 - \phi_2)].
 \end{aligned} \tag{18}$$

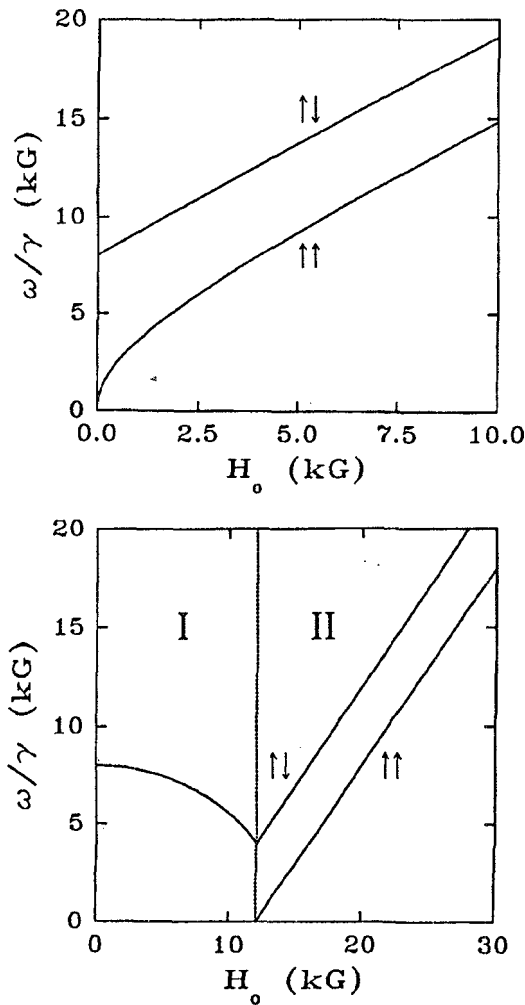


Figure 2: The dispersion relations for a system consisting of two identical parallel coupled ferromagnetic layers with the external field applied top) in the plane of the film; bottom) normal to the film plane. The values of parameters used in this figure are $H_u = -12$ kG and $H_{ex} = 2.0$ kG. The $\uparrow\uparrow$ represents the acoustic mode and $\uparrow\downarrow$ is the optical mode.

The equilibrium orientation of the magnetization in each layer can be obtained from Eq. (5). For an easy

plane material, $K_{2u,i}^{eff} < 0$, when the magnetic field is applied in the plane of the structure along the x -axis, the magnetization in both layers will be oriented along the direction of the applied field. Thus the hysteresis loop for the coupled system will be the same as that for the uncoupled system in this geometry.

When the magnetic field is applied normal to the film, y -axis, the applied field must work against the torque induced by the uniaxial/demagnetization energy. In the case that the two ferromagnetic layers have different effective anisotropy fields $H_{u,i} = 2K_{2u,i}^{eff}/M_i$, the magnetization in each film will not always be parallel to each other below the saturation field. As a result the applied field must also work against the torque induced by the interlayer exchange energy, A_{12} . Only when $H_{u,1} = H_{u,2} = H_u$, the equilibrium orientation of \mathbf{M}_1 will always be parallel to \mathbf{M}_2 and independent of the exchange energy. The y -component of the magnetization in this case will have a simplified form

$$M_y = M(-H_0/H_u) \tag{19}$$

and the film becomes saturated when $H_0 = -H_u$. Again this equilibrium orientation is the same condition expected for a single ferromagnetic film.

The dispersion relations can be obtained from Eq. (6) by letting $N = 2$ and assuming that the response of the rf magnetization is of the form $\exp(i\omega t)$. A typical example of the dispersion curve, ω/γ , versus the applied magnetic field, H_0 is shown in Figure 2 at both the parallel orientation, $\mathbf{H}_0 \parallel x$ and the perpendicular orientation, $\mathbf{H}_0 \parallel y$ assuming that the properties of the two ferromagnetic layers are identical (i.e. $M_1 = M_2 = M$, $H_{u,1} = H_{u,2} = H_u$ and $t_1 = t_2 = t$). One of the modes will have the magnetization in each film precessing in phase with the same amplitude ($m_{\theta,1} = m_e$, and $m_{\phi,1} = m_{\phi,2}$), the acoustic mode ($\uparrow\uparrow$), and the dispersion relation is the same as that for the individual ferromagnetic layers as if they were to remain uncoupled

$$\frac{\omega}{\gamma} = \sqrt{H_0(H_0 - H_u)} \quad (\mathbf{H}_0 \parallel x)$$

and
$$\frac{\omega}{\gamma} = H_0 + H_u \quad (H_0 > -H_u) \quad (\mathbf{H}_0 \parallel \mathbf{y}) \quad (21)$$

In the other mode, the rf magnetization of the two layers will precess with the same amplitude but in the opposite direction ($m_{\theta,1} = -m_{\theta,2}$ and $m_{\phi,1} = -m_{\phi,2}$), the optical mode ($\uparrow\downarrow$). The frequency of the optical mode is shifted to a higher value due to the additional torque introduced from the exchange coupling term because the magnetization in each individual layers is not oriented parallel to each other during the precession. The dispersion relation in the saturation region will have the same form as in Eq. (20) if the external field, H_0 , is replaced by $H_0 + 2H_{ex}$, where the exchange field is defined as $H_{ex} = A_{12}/tM$. Below the saturation region with the applied field normal to the film, the resonance frequency of the optical mode remains at high values and decreases with the increase of the field. The dispersion relation of the optical mode in this region will be

$$\omega/\gamma = \frac{2H_{ex}(2H_{ex} - H_u + H_0^2/H_u)}{H_u} \quad (22)$$

The intensity of each mode can be calculated from Eq. (17). The acoustic mode will have a large intensity while the intensity of the optical mode will be zero. As a result the optical mode will not be excited by a uniform rf field. One way to overcome the difficulty is to make samples with different thicknesses in each layer. However the intensity of the optic mode will still be zero if the thickness difference between the two layers does not produce a difference of the effective anisotropy field

$H_{u,i}$ from one layer to another^{7,23}, because the amplitude of the rf magnetization in each layer is inversely proportional to the film thickness. In most systems, the effective uniaxial anisotropy field $H_{u,i}$ will change with the change of the film thickness. As mentioned before, one of the main contributions to the uniaxial anisotropy energy comes from the surface anisotropy energy which will produce a $1/t$ dependence of the effective field. When the magnetic layer thickness is on the order of 10 Å, the change of the effective anisotropy field $H_{u,i}$ (several kG) due to the change of the film thickness (several Å) will be large enough to see a weak optic mode on the high frequency or low magnetic field side of the acoustic mode.

11.3 Antiparallel Coupled Ferromagnetic Bilayer System

In the case of anti-parallel coupling between the ferromagnetic layers, the sign of the exchange coupling coefficient, A_{12} , changes. While this is a subtle change in the equations of motion it has a profound effect on the equilibrium orientation of the magnetization in the two ferromagnetic layers as well as on the dispersion relation.

For two ferromagnetic films coupled anti-parallel and having a uniaxial anisotropy energy normal to the film, $K_{2u}^{eff} < 0$, as well as an in-plane uniaxial anisotropy of the form given by Eq. (14), the energy density can be expressed as

$$\begin{aligned} E = & -\mathbf{H}_0 \cdot (t_1 \mathbf{M}_1 + t_2 \mathbf{M}_2) - \left(t_1 K_{2u,1}^{eff} \frac{M_{y,1}^2}{M_1^2} + t_2 K_{2u,2}^{eff} \frac{M_{y,2}^2}{M_2^2} \right) \\ & - \left(D_1^x t_1 \frac{M_{x,1}^2}{M_1^2} + D_2^x t_2 \frac{M_{x,2}^2}{M_2^2} \right) - A_{12} \frac{\mathbf{M}_1 \cdot \mathbf{M}_2}{M_1 M_2} \\ = & -H_0 [t_1 M_1 \sin \theta_1 \cos(\phi_1 - \phi_H) + t_2 M_2 \sin \theta_2 \cos(\phi_2 - \phi_H)] \\ & - (K_{2u,1}^{eff} t_1 \sin^2 \theta_1 \sin^2 \phi_1 + K_{2u,2}^{eff} t_2 \sin^2 \theta_2 \sin^2 \phi_2) - (D_1^x t_1 \sin^2 \theta_1 \cos^2 \phi_1 \\ & + D_2^x t_2 \sin^2 \theta_2 \cos^2 \phi_2) - A_{12} [\cos \theta_1 \cos \theta_2 + \sin \theta_1 \sin \theta_2 \cos(\phi_1 - \phi_2)] \end{aligned} \quad (23)$$

The external field \mathbf{H}_0 is assumed to lie in the $\mathbf{x} - \mathbf{y}$ plane and the exchange coupling constant, A_{12} , is less than zero.

As in the parallel coupled system the equilibrium orientation of the magnetization of each layer can be obtained from Eq. (5). Assuming again that each layer is identical, $M_1 = M_2 = M$, $K_{2u,1}^{eff} = K_{2u,2}^{eff} = K_{2u}^{eff}$, $t_1 = t_2 = t$ and $D_1^x = D_2^x = D^x$, the application of

the external field along the easy axis ($\mathbf{H}_0 \parallel \mathbf{x}$) will produce three different sets of conditions for the magnetization. For increasing magnetic field, the first region is in the range $0 \leq H_0 \leq \sqrt{H_D(2H_{ex} + H_D)} = H_{\uparrow}$, where $H_D = 2D^x/M$ is the in-plane anisotropy field and $H_{ex} = |A_{12}|/tM$ is the exchange field acting on each layer. In this field range the magnetization of the films continue to lie along the $\pm x$ -axis. At the spin flop

field for increasing magnetic fields, $H_0 = H_1$, the spins reorient toward the direction perpendicular to the field along the $\pm z$ -axis but canted toward the x -axis at the angle $\theta_1 = \pi - \theta_2 = \sin^{-1}[H_0/(2H_{ex} - H_D)]$. In the second region the spins remain canted until the field has reached the saturation field $H_0 = H_{\parallel, sat} = 2H_{ex} - H_D$, at which value the spins lie parallel to the x -axis in the saturation state. The third range of field values is for $H_0 > H_{\parallel, sat}$ for which the magnetization is always along the direction of the magnetic field.

For decreasing magnetic field the spin flop occurs at a lower field value of $H_1 = \sqrt{H_D(2H_{ex} - H_D)^2/(2H_{ex} + H_D)}$. This results in a hysteresis about the vicinity of the spin-flop field²⁶. The magnitude of the x component of the net magnetization as a function of the external field applied along the x -direction is shown in Figure 3.

When the magnetic field is applied normal to the film, ($H_0 \parallel y$), the spins are forced to rotate about the z -axis toward the y -axis within the x - y plane and a spin-flop condition is not observed. The equilibrium condition from Eq. (5) gives the condition $\phi_1 = \pi - \phi_2 = \sin^{-1}[H_0/(2H_{ex} + H_D - H_u)]$. Under these conditions, the net magnetization along the y -axis is proportional to the external field until the applied field reaches the saturation value $H_0 = 2H_{ex} + H_D - H_u = H_{\perp, sat}$ above which the net magnetization along the field direction remains saturated at M .

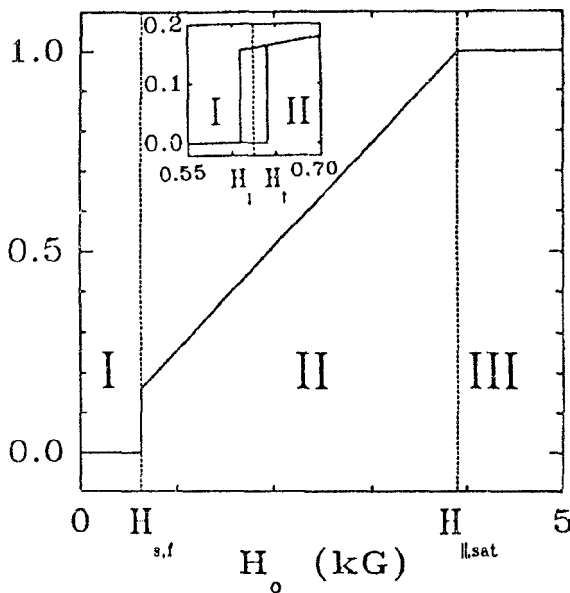


Figure 3: The in-plane component of the magnetization as a function of the field strength for a pair of anti-parallel coupled ferromagnetic films when the applied field is in the plane and parallel to the in-plane anisotropy field ($H_0 \parallel x$ -axis). The values of the parameters used are $H_u = -12$ kG, $H_{ex} = 2.0$ kG and $H_D = 0.1$ kG. The inset figure shows the hysteresis in the vicinity of the spin-flop field.

Though in the easy plane multilayer system, $K_{2u}^{eff} <$

0, only the canted and saturation regions exist in the hysteresis loop with the external field normal to the film, the spin-flop condition can be observed²⁷ for the system with easy axis normal to the film, $K_{2u}^{eff} > 0$. In this orientation the spins will stay along the $\pm y$ -axis until the external field is large enough to force the spins to reorient anti-parallel in the film plane but canted toward the direction of the external field (y -axis). Because the effective uniaxial anisotropy field, H_u , is of the order of $1 \sim 10$ kG, the separation between the spin-flop field with increasing magnetic field, H_1 , and that with decreasing magnetic field, H_2 , will be of the order of 1 kG, much larger, than that shown in Figure 3 for parallel orientation.

Using the form of the energy given in Eq. (22), the equation of motion for the system as given in Eq. (6) can be obtained. For the parallel orientation, $H_0 \parallel x$ -axis, the dispersion relation is shown in Figure 4. In region I, below the spin-flop field, the dispersion relation is significantly modified from that of a bulk antiferromagnetic material.

In a bulk antiferromagnetic material, the dispersion relation is given by the equation²⁸

$$\frac{\omega}{\gamma} = \sqrt{H_D(2H_{ex} + H_D)} \pm H_0 \approx \sqrt{2H_{ex}H_D} \pm H_0, \quad (24)$$

where H_{ex} , is the exchange field that arises from the exchange interaction between the magnetic moments on the two sublattices. In most antiferromagnetic materials the exchange field is orders of magnitude larger than the anisotropy field, H_D , so the approximation in Eq. (23) is the usual expression for dispersion relation. If an external magnetic field is applied along the easy axis direction, the degeneracy of the two modes at zero field is lifted. One mode increases in frequency while the other decreases with the field H_0 as indicated in Eq. (23).

For anti-parallel coupled films the situation is quite different in that each ferromagnetic layer has the added torque due to the magnetostatic energy contribution. The effect of this added torque is to lift the degeneracy in the zero field modes as shown in Figure 4. The low frequency mode decreases to zero frequency while the high frequency mode increases slightly as the field approaches the spin-flop field. At the spin-flop field there is a discontinuity in the high frequency mode but in addition the position of the acoustic mode and the optic mode interchange regions. As the applied field is further increased in region II, the frequency of the acoustic mode increases but with a significantly different behavior than that observed for the case of a single layer ferromagnetic film (see the dashed curve in Figure 4). At the same time the frequency of the optical mode decreases and reaches zero at the saturation field. In the saturation region, the acoustic mode is degenerate with that of the ferromagnetic resonance for a single

layer while the optical mode is shifted to the low frequency or high magnetic field side by the field, $2H_{ex}$. The dispersion relations in each region are given by the following equations:

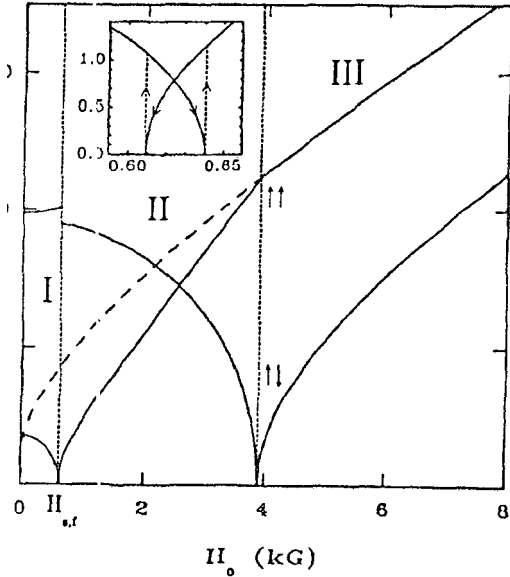


Figure 4: The dispersion relations for the same condition as Figure 3. The notations of $\uparrow\uparrow$ and $\downarrow\downarrow$ are the same as those in Figure 2. The value of $g = 2$ is used along with other parameters as described in Figure 3. The dashed line is the behavior expected for a single ferromagnetic layer. The inset figure shows the hysteresis of the resonance frequency in the vicinity of the spin-flop field.

In region I:

$$\left(\frac{\omega}{\gamma}\right)_{\pm}^2 = H_0^2 - H_D^2 + (H_D + H_{ex})(2H_D - H_u) \pm [H_0^2(2H_D - H_u) \times (2H_D - H_u + 4H_{ex}) + H_{ex}^2 H_u^2]^{1/2} \quad (25)$$

In region II:

$$\left(\frac{\omega}{\gamma}\right)_{\pm}^2 = [2H_{ex}^2 + H_D(H_{ex} - H_u)]\sin^2\theta + (H_{ex} - H_u)(H_{ex} - H_D) - H_{ex}^2 \pm H_{ex}[(2H_{ex} - 2H_u + H_D)\sin^2\theta - (H_D - H_u)] \quad (26)$$

where $\sin\theta = H_0/(2H_{ex} - H_D)$.

In region III

$$\left(\frac{\omega}{\gamma}\right)_{\pm}^2 = (H_0 + H_D - H_{ex} \pm H_{ex})(H_0 - H_u + H_D - H_{ex} \pm H_{ex}) \quad (27)$$

When the field is applied normal to the film, $H_0 \parallel y$ -axis, the dispersion relation is shown in Figure 5. In region I the acoustic mode maintains its high frequency

status while the optical mode is at low but finite frequency. The shift of the optical mode from zero is due to the weak in-plane anisotropy field, H_D . At saturation and in region II, the acoustic mode is again degenerate with the normal ferromagnetic resonance and the optical mode remain at a field, $2H_{ex}$, higher than that of the acoustic mode as expressed by the equations:

In region I:

$$\left(\frac{\omega}{\gamma}\right)_{\pm}^2 = -H_{ex}^2 \cos 2\phi + (H_{ex} + H_D)[H_{ex} + (H_D - H_u)\cos^2\phi] \pm \{H_{ex}[H_{ex} + (H_D - H_u)\cos^2\phi - (H_{ex} + H_D)\cos 2\phi]\} \quad (28)$$

where $\sin\phi = H_0/(2H_{ex} + H_D - H_u)$.

In region II:

$$\left(\frac{\omega}{\gamma}\right)_{\pm}^2 = (H_0 + H_u - H_D - H_{ex} \pm H_{ex})(H_0 + H_u - H_{ex} \pm H_{ex}) \quad (29)$$

As opposed to the case for parallel coupling between the layers, for anti-parallel coupling the optical mode is observed at lower frequencies. This shift to lower frequencies is due to the decrease in the exchange energy as the magnetizations in the two layers deviate from the parallel orientation as opposed to the increase in energy for the parallel coupled case, $A_{12} > 0$. Thus in the CFFR experiments, the low field mode should have the stronger absorption while the high field mode, the optical mode, will have zero intensity for identical layers and a weak intensity if the layers have small difference in either M or their internal energy.

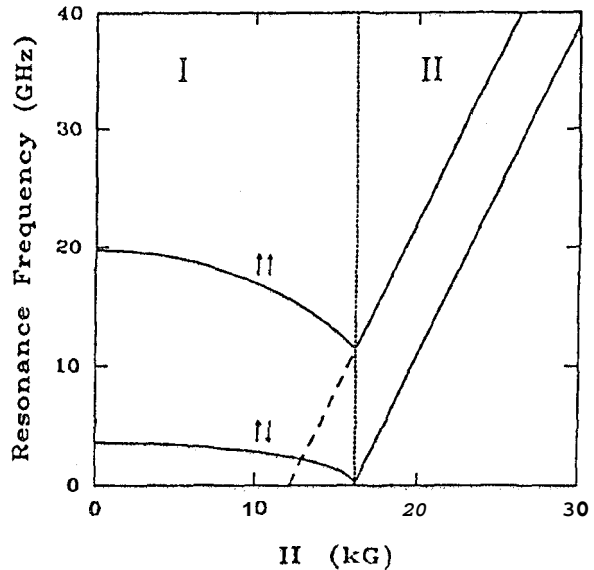


Figure 5: The dispersion relations for the same condition as Figure 5 with the exception that the magnetic field is applied normal to the plane of the film. Again the dashed line is the dispersion curve predicted for the single ferromagnetic layer.

11.4 Multilayer Films

In a system with N ferromagnetic/"non-magnetic" periods, the dispersion relations can be obtained from Eq. (6). Assuming that the N ferromagnetic layers are identical and the exchange coupling coefficients between each adjacent layers are the same, $A_{i,i\pm 1} = A_{12}$, the system will have N normal modes whose "wave function" will vary sinusoidally across the film layers and have a natural boundary condition (zero slope) at the surface of the structure. The "fundamental mode" for this set of boundary conditions will have all the ferromagnetic layers precessing in phase with the same amplitude, the uniform mode.

In the case of parallel coupling between the layers, the high order spin wave modes will occur at the high frequency or low magnetic field side of the uniform mode. The highest frequency or lowest field mode, will correspond to that of the optic mode discussed in the trilayer system with the rf magnetization precessing anti-parallel to each other between the i th and $(i\pm 1)$ th layer. In the saturation region, the field separation between the optic mode and the uniform mode is in the range of $2H_{ex} \leq \Delta H_{res} \leq 4H_{ex}$, with $\Delta H_{res} = 2H_{ex}$ for $N = 2$ and ΔH_{res} approaching $4H_{ex}$ when the number of periods approaches infinity.

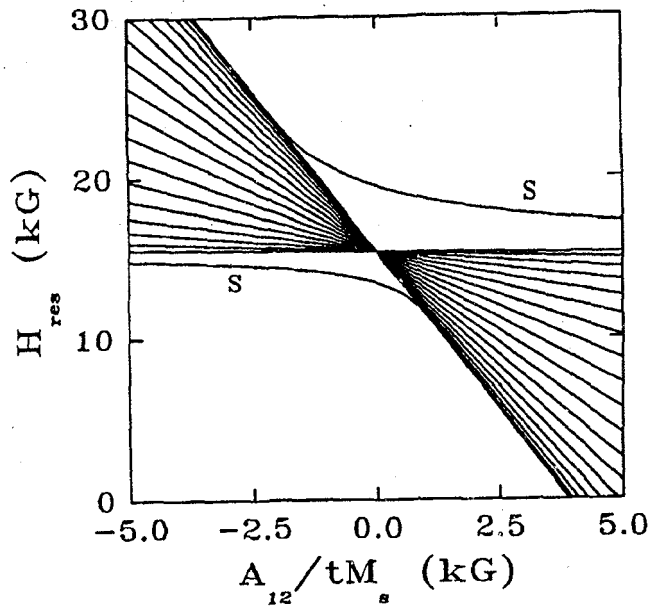


Figure 6: The spin-wave resonance modes for a set of 20 periods of magnetic/"non-magnetic" layers as a function of the strength of the exchange interaction when the field is applied normal to the film. The values of the parameters used are $H_{u,1} = -16$ kG, $H_{u,i} = -12$ kG where $i = 2, \dots, 19$, $H_{u,20} = -10$ kG and $\omega/\gamma = 3.5$ kG. The "surface" like modes are labeled with a "S".

In the case of anti-parallel coupling between the layers, the N normal modes will again lie between the values of the uniform mode (or acoustic mode) and the

optic mode. However, in the saturation region, the high order spin wave modes will occur at the low frequency or high field side because the out of phase rf magnetization resonance will reduce the interlayer exchange energy.

For all but the uniform mode, the precession of each layer will have a systematic variation of amplitude and phase from layer to layer such that the net transverse rf dipole moment of these modes will be zero and therefore will not be excited by a uniform rf field.

In many instances, the surface ferromagnetic layers will have a different environment due to the broken symmetry. As a result, the energy expressions for \mathcal{E}_1 and \mathcal{E}_N may be quite different from those in the "bulk" of the structure. Depending on the nature of \mathcal{E}_1 and/or \mathcal{E}_N , a pinned or unpinned^{13,29} boundary may exist. For a pinned boundary condition, the lowest order mode will be a sinusoidal mode for parallel coupling ($A_{12} > 0$) while it will have an exponential "surface" like mode for anti-parallel coupling ($A_{12} < 0$). For an unpinned boundary condition, the "surface" like mode can only be observed in the parallel coupled multilayer system. Figure 6 shows the resonance fields as a function of the exchange field, A_{12}/tM_s , at X-band, $\omega/\gamma = 3.5$ kG, with the applied field normal to the film for a 20 periods multilayer film. The film is assumed to have an unpinned boundary condition in the first layer and a pinned boundary condition in the 20th layer.

These results show that CFFR spectra can be a very sensitive probe of the internal energies of each layer as well as the interlayer exchange coupling strength.

III. Experimental Results

CFFR experiments have been carried out on many multilayer systems with the structure $(TM/NM)_N$, where TM is the ferromagnetic transition metal layer such as Co, Fe, Ni or their alloys and NM is the "non-magnetic" metal such as Pt, Pd, Cr, Cu, Ag, Ru and Au. The research has concentrated on the internal anisotropy energy within each magnetic layer and the interlayer exchange coupling as a function of both the magnetic layer thickness and the "non-magnetic" layer thickness. Temperature dependence of those properties has also been studied.

11.1.1. Internal Anisotropy Energies

The internal energies having the form expressed by Eq. (8) through (15) have been determined for a number of structured systems by the study of angular dependence of the CFFR spectra. The cubic crystalline anisotropy energy, showing a 4-fold anisotropy energy in the film plane, can be observed in some of the MBE grown single-crystal samples. A typical resonance field as a function of the orientation of the external field within the field plane is shown in Figure 7. Heinrich, *et al.*^{7,19,23,30,31} determined the cubic crystalline anisotropy energy constants K_1 for several systems

such as Fe(001)/Ag(100), Ni(001)/Fe(001)/Ag(001), Co(001)/Cu(001) and Fe(001)/Cu(001)/Fe(001). In the case of single crystal Fe layer deposited on Ag substrate, K_1 decreases dramatically from that of the bulk Fe value when Fe layer thickness is less than 10 Å. The deposition of an extra Ni overlayer (> 6 monolayer) on top of the Fe layer enhanced the cubic crystalline anisotropy energy by an order of magnitude due to the lattice reconstruction in the Fe/Ni bilayers. Similar effects has not been found if the Ni layer is replaced by Cu. A negative value of the cubic anisotropy field, $2K_1/M$, was observed to be about -1 kG in the Co(001)/Cu(001)/Co(001) structures. The cubic anisotropy energy increases with the decrease of temperature and nearly double the room temperature value at 77 K.

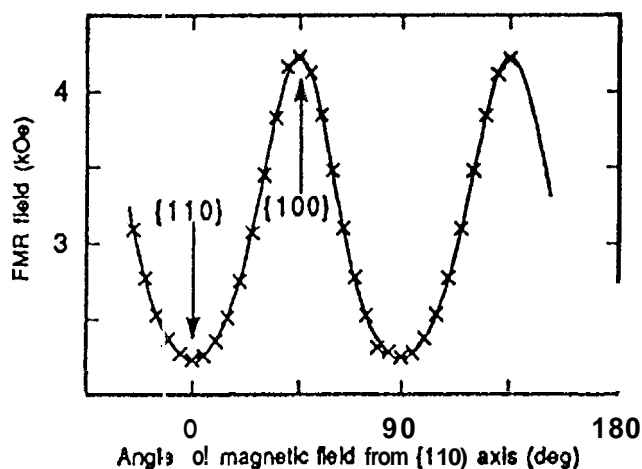


Figure 7: In-plane angular dependence of the FMR field observed for the $(Co)_4_3/(Cu)_6/(Co)_4$ sample, where the subscript is in monolayers. The solid line represents a theoretical fit using the following magnetic values: $H_u = -40.8$ kG, $2K_1/M = -1.05$ kG, $f = 36.3$ GHz, and $g = 2.16$. (from Ref. 30)

In a 40 Å Fe(001)/Cr(001)/40 Å Fe(001) structure, Krebs et al.^{25,32} observed as many as five resonance modes at some microwave frequencies with the external field applied along the $[1\bar{1}0]$ direction in the film plane. The complex spectra were explained using the cubic anisotropy energy along with the interlayer exchange coupling between the two Fe layers as shown in Figure 8. It was reported that the cubic anisotropy field, $2K_1/M$, is independent of the Cr thickness in the range $12\text{Å} < t_{Cr} < 25\text{Å}$ and the values are close to that of the bulk Fe.

The dominant term in the CFFR spectra is the effective uniaxial anisotropy energy normal to the film, including the demagnetization energy, the internal bulk uniaxial anisotropy energy and the surface anisotropy energy as expressed in Eq. (12) and (13). From a series of 275 Å Ag/Fe/550 Å Ag structures for Fe layer thickness of 24 Å, 48 Å and 80 Å, Hurdequint, et al.¹⁵ determined the surface anisotropy energy, K_{sur} , between

each Fe/Ag interface to be 1.05 erg/cm^2 . In a $(Fe/Pt)_N$ multilayer structure where $N=35$ or 50, Wigen, et al.¹⁶ reported a surface anisotropy energy of 0.14 erg/cm^2 for the Fe thickness of 5 Å, 7 Å and 15 Å with Pt thickness constant at 15 Å. Purcell, et al.¹⁷ investigate the internal field for Co/Pd(111) structures for which a 9 monolayer film of Pd was deposited on Co layers that varied from 5 to 12.5 monolayers. The observed value of K_{sur} was found to be 0.8 erg/cm^2 .

Zhang, et al.^{18,29} investigated the development of the induced uniaxial anisotropy energy as a function of the Pt thickness in Co/Pt multilayer films. For a series of Co/Pt structure having 20 periods, the Co layers were 25 Å thick and the Pt layers varied from 1 Å to 18 Å. The evolution of the anisotropy energy was observed to depend on the Pt interlayer thickness as

$$K_{2u} = K_{2u}^b + \frac{2K_{sur}^0}{t_{Co}} [1 - \exp(-\frac{t_{Pt}}{t_0})] \quad (30)$$

The exponential term accounts for the dependence of the surface anisotropy energy on the thickness of the Pt layer. The value of t_0 is 13 Å and the value of surface anisotropy energy, K_{sur}^0 , for this Co/Pt structure is 0.91 erg/cm^2 .

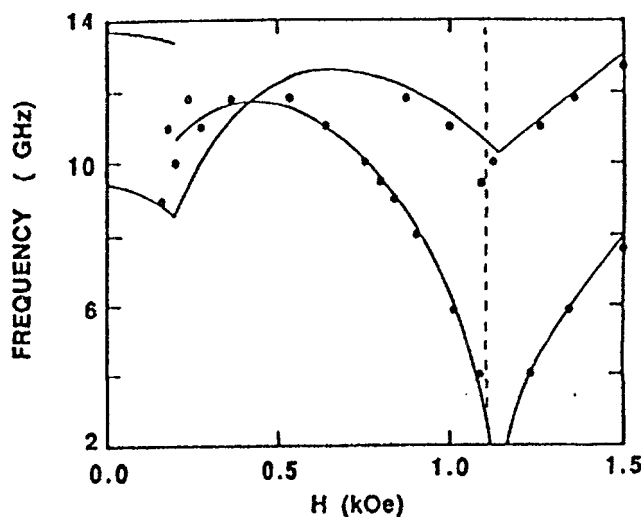


Figure 8: Multiple-frequency FMR data for the (40 Å Fe/13 Å Cr /40 Å Fe) thin film sample with the external field parallel to the hard axis in the film plane $[1\bar{1}0]$. The solid curves are the result of resonance mode calculations using the following parameters: $H_K = 2K_1/M = 520$ G, $A_{12}/tM = -300$ G and $H_D = 2D/M = 10$ G. The dashed line marks the saturation field. (from Ref. 25)

The contribution from the surface anisotropy energy will become larger than that of the magnetostatic energy when the thickness of the magnetic layer decreases to a critical value, t_c . For films with the magnetic layer thinner than t_{cr} a perpendicular magnetic anisotropy

property, $K_{2u}^{eff} > 0$, will be obtained and the magnetization will be oriented normal to the film. In Co/Pt and Co/Pd multilayer structures^{17,18}, the transition thickness is about $10 \sim 15 \text{ \AA}$.

Artman, *et al.*³³ measured the angular dependence of the CFFR in a number of Co/Pt multilayer films and observed that the fourth order uniaxial anisotropy energy constant, K_{4u} , as expressed in Eq. (11), cannot be neglected in the system when the second order term K_{2u}^{eff} is close to zero. Over a series of seven different films having various thicknesses of the Co and the Pt, there appeared to be no consistent variation in the values of the fourth order anisotropy field, $4K_{4u}^{eff}/M$, which is in the range of $0 \sim 1 \text{ kG}$.

111.2. Interlayer Exchange Coupling

The important difference between the coupled multilayer system and the single layer system is the existence of the exchange modes. The advantage of using CFFR and Brillouin light scattering is the ability to observe the exchange modes predicted in the previous section and to evaluate the sign and magnitude of the exchange coupling constant, $A_{i,i+1}$. Those exchange modes have been observed in many multilayer systems such as Fe/Cr^{1,2,12,25,32}, Fe/Cu^{7,31,34-36}, Fe/Ag^{19,36}, Fe/Au^{12,36}, Fe/Pd^{9,35-37}, Fe/Pt¹⁶, Fe/C³⁸, Co/Cu³⁰, Co/Pd^{8,10}, Co/Pt^{18,29,39}, Co/Ru^{27,40}, Ni_xFe_{1-x}/Cr^{11,41}, Ni_xFe_{1-x}/Cu^{11,41,42}, Ni_xFe_{1-x}/Pd^{11,41} and Ni_xFe_{1-x}/Ag/Ni^{11,43}.

As mentioned before, the interlayer layer exchange coupling constant, A_{12} , is proportional to the resonance field separation of the acoustic mode and the optical mode, ΔH_{res} , in a system with two identical magnetic layers separated by the "non-magnetic" layer. However the optic mode can not be observed in the CFFR spectra unless a difference of the effective uniaxial anisotropy field, ΔH_{2u}^{eff} , is created between the two magnetic layers. As a result, the separation between the two modes, $\Delta H_{res}(A_{12}, \Delta H_{2u}^{eff})$, does not only depend on the interlayer exchange coupling constant but also on the difference of the effective uniaxial anisotropy field. A_{12} can be obtained when ΔH_{2u}^{eff} is known or if it is so small compared with the exchange field, $2A_{12}/tM$, that it can be neglected. The former condition can be achieved by making two separated single layer films with similar structure as that in the trilayer system and measure the internal anisotropy energy for each film. The latter condition will be satisfied if the intensity of the acoustic mode is at least an order of magnitude larger than that of the optical mode. Otherwise the intensity expressed in Eq. (17) as well as the resonance fields must be used to calculate A_{12} properly. In a multilayer structure with $N > 2$, the exchange constant, $A_{i,i\pm 1}$ can be evaluated from the field or frequency dependence of the "spin-wave" like higher order exchange modes.

Of the systems investigated to date, Pt and Pd interlayers have a positive exchange coupling constant producing a parallel coupling between the ferromagnetic layers for all values of the thickness. Bloemen, *et al.*³⁹, investigated the trilayer films of Co/Pt/Co with the Pt layer thickness varied from 4 \AA to 100 \AA . The thickness of the Co layers are 50 \AA and 20 \AA respectively so as to produce an anisotropy difference in each Co layer. The effective anisotropy fields for each layer were chosen to give a best fit of the resonance fields for a total of 8 samples. The in-phase and out-of-phase modes can be observed only in films with Pt layer thickness greater than 20 \AA . The exchange constant A_{12} was found to decrease with the increase of the Pt thickness as shown in Figure 0.

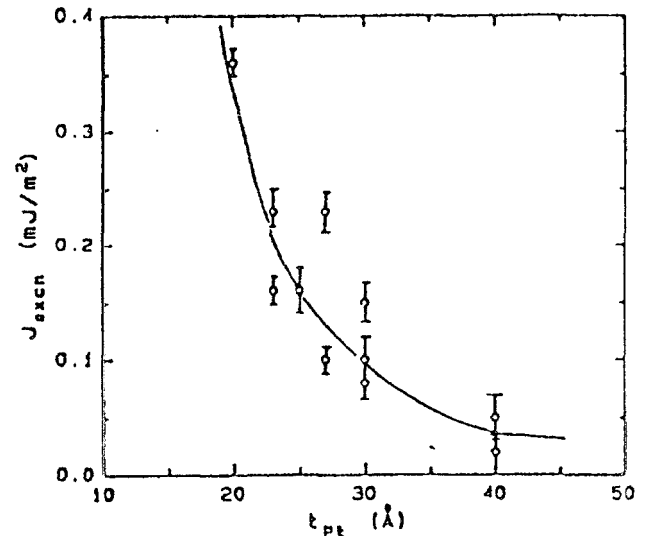


Figure 0: Interlayer exchange energy J_{exch} (the same as A_{12}) as a function of the Pt spacer thickness. (from Ref. 39)

In a series of $(\text{Co/Pt})_{20}$ structures investigated by Ziang, *et al.*^{18,29}, the first Co layer of the structure was deposited on a Ru buffer layer. This removes one of the Pt interface contributions to the uniaxial anisotropy energy in layer one, which depends on the Pt thickness and is on the order of 5 kG for $t_{Pt} \geq 10 \text{ \AA}$. As a result the effective anisotropy energy in layer one is different from those of bulk layers as the Pt layer develops. This produces an unpinned surface condition with the external field normal to the film. Two modes, the "surface like" mode and the first order spin-wave exchange mode, were observed for the films with Pt thickness greater than 4 \AA . From the analysis of the positions and intensities of the modes in the CFFR spectra it was possible to determine the exchange coupling coefficient as a function of the Pt thickness in the range of $4 \text{ \AA} \leq t_{Pt} \leq 18 \text{ \AA}$. The relation was found to have an exponential dependence

$$A_{12}(t_{Pt}) = A_{12}^0 \exp(-\epsilon), \quad (31)$$

where A_{12}^0 was measured to be 70 erg/cm^2 and t_0 to be 7 \AA for this series.

Bosse, *et al.*⁴¹ investigated two permalloy ($\text{Ni}_{80}\text{Fe}_{20}$) films separated by different "non-magnetic" layers such as Pd, Cu, and Cr. The exchange coupling across Pd and Cu follows the same exponential relation as expressed in Eq. (30). with a greater decay length for Pd.

Cielinski, *et al.*³⁷ studied a series of Fe/Pd/Fe trilayer films grown by MBE. A weak optical mode was observed in films with the Pd thickness greater than 5 monolayer. The exchange coupling constant evaluated from the resonance fields reveals an oscillatory behavior superimposed on the exponential decreasing background. The oscillation period, 4 monolayer, is larger than that predicted from the layered RKKY interactions.⁴⁴

In contrast to Pt and Pd, the metals such as Cu, Ag, Au, Cr, and Ru produce exchange coupling coefficients that oscillate between positive and negative values to produce parallel or anti-parallel coupling between the magnetic layers as a function of the thickness of the "non-magnetic" layer. In a Fe/Cr/Fe trilayer structure for which the Fe layers were 110 \AA and the Cr varied from 2 to 20 \AA , Barnas, *et al.*¹² determined the sign and magnitude of the exchange coupling constant from the positions of the two resonance frequencies in the Brillouin light scattering spectra, taking into account the exchange energy within each Fe layer as well. The interlayer coupling changes sign from parallel coupling at $t_{Cr} < 7 \text{ \AA}$ to anti-parallel coupling at $t_{Cr} > 7 \text{ \AA}$. The coupling coefficient vanishes at $t_{Cr} \approx 17 \text{ \AA}$. Using CFFR technique, Krebs, *et al.*²⁵, investigated another Fe/Cr/Fe series for which the Fe layer was 40 \AA thick and the Cr varied from 4 to 85 \AA . Multimodes were found in the resonance spectra that were consistent with anti-parallel coupling for Cr thickness between 13 \AA and 24 \AA . A maximum exchange field of about 300 G was obtained at $t_{Cr} \approx 16 \text{ \AA}$. No antiferromagnetic alignment was shown in both the $t_{Cr} < 13 \text{ \AA}$ region and the $t_{Cr} < 24 \text{ \AA}$ region.

In a series of Fe/Cu, Ag, Au/Fe trilayer structures, Cielinski, *et al.*³⁶, observed an oscillation from parallel to anti-parallel coupling as a function of the Cu thickness with a periodicity of ~ 10 monolayer. The amplitude of the coupling constant decreases with increasing Cu thickness and the values at 77 K are almost double those at room temperature. The oscillations in the Ag and/or Au included structures were much weaker compared with those of Fe/Cu/Fe structures and the coupling constant decreases rapidly to zero as the thickness exceeds 6 to 10 monolayers.

Zhang, *et al.*⁴⁰ have investigated Co/Ru/Co trilayers and for Ru layer thicknesses on the order of 10 \AA , a very strong anti-parallel coupling between the Co layers is observed for which the acoustic mode and the optic mode could be separated by as much as 4000 G . These

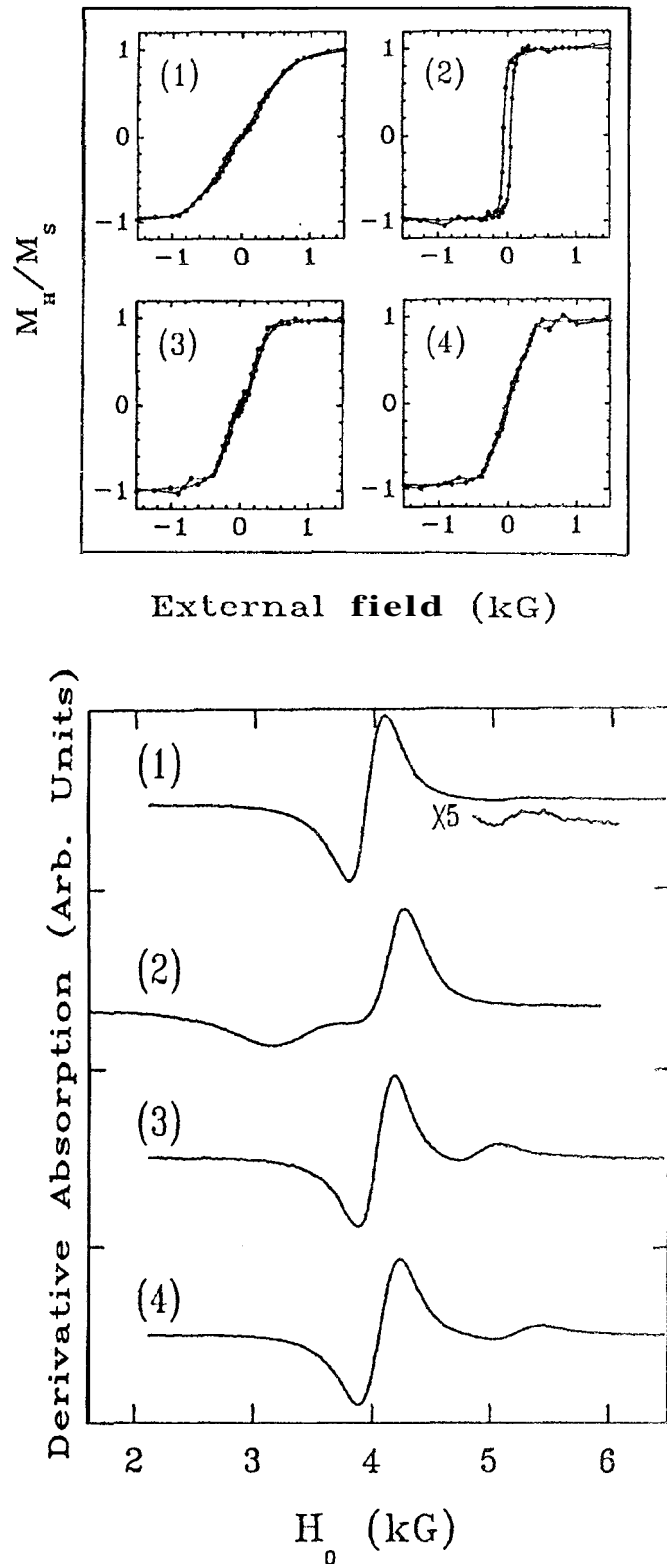


Figure 10: top) In-plane magnetization measurement as a function of the field strength for the structure of (32 \AA Co/Ru/ 32 \AA Co) trilayers. The Ru thicknesses are (1) 15 \AA , (2) 20 \AA , (3) 25 \AA and (4) 30 \AA . bottom) CFFR spectra at 22.9 GHz with the magnetic field applied in the film plane. The samples are the same as those mentioned in part a). (from Ref. 40)

values are about an order of magnitude larger than that observed in the other typical structures. The spectra as well as the magnetization hysteresis loop has clearly shown an oscillation behavior of the coupling constant from positive to negative with the change of Ru thickness (see Figure 10).

The temperature dependence of the exchange coupling constant, A_{12} , for a Fe/Pd/Fe structure has been studied by Heinrich, et al.⁹. A_{12} increases with the decrease of temperature, following a Curie-Weiss type of dependence

$$A_{12} \propto 1/(T + \Theta) \quad (32)$$

with Θ on the order of 50 K.

11.1.3. Miscellaneous Effects

Hurdequin, et al.⁴⁵, investigated the line shape and relaxation processes in Fe/Ag multilayer structures. For the in-plane or parallel orientation for CFFR resonance the ratio of the slopes of the absorption line of the high field to the low field side of the line, A/B , was found to vary between 0.7 and 1.0 for the whole series of films. This corresponds to a positive signal phase and the effect cannot be explained by the eddy current contributions for which the A/B ratio should be greater than unity. The details of the mechanism responsible for this effect remains to be explained. The linewidth of the resonance modes were consistent with a mechanism in which the magnetic energy is carried away (relaxed) by the conduction electrons. In Ag, the spin diffusion length would have a value $\delta_{eff} = (2DT_2)^{1/2}$, with D the electron diffusion constant and T_2 the transverse spin relaxation time. From the analysis a diffusion length of 500 to 1000 Å is determined which is in reasonable agreement with results obtained by other techniques in Ag metals.

Heinrich, et al.²³, observed that the linewidth of the CFFR spectra as a function of the resonance frequency for a MBE grown Ni/Fe bilayer structure with a large 4-fold in-plane anisotropy energy follows the relation

$$\Delta H_{res} = \Delta H_0 + A\omega, \quad (33)$$

where ΔH_0 originates in the inhomogeneities of the sample and the frequency dependent part is caused by the intrinsic Gilbert damping as expressed in Eq. (16). The damping related parameter A was nearly isotropic while ΔH_0 was sensitive to the direction of the external field. ΔH_0 was almost four times larger with the external field along the hard direction in the film plane than that with the external field along the easy axis. This was explained to be a result of crystalline defects generated during the Ni overlayer lattice relaxation. In another structure with a single Fe(100) film grown on Ag(001) substrate¹⁹, the same group reported a rapid increase, almost an order of magnitude, in the Gilbert damping coefficient with decreasing Fe thickness from 40 Å to 4 Å. Enhanced spin-orbit coupling for thinner

Fe films was proposed to be the reason for the increase of the Gilbert damping parameter.

IV. Conclusions

The magnetic properties of the magnetic/"non-magnetic" multilayer structures have been widely studied by the CFFR technique. The intrinsic magnetic parameters, such as the internal uniaxial anisotropy energy and the exchange coupling constant, varied from one series to another depending on the structure of the sample, the thickness of each layer and the sample preparation conditions. While it is not possible to "catalog" all of the results in a convenient form, there are a few generalities that can be proposed.

(1) In most of the structures, the internal uniaxial anisotropy energy of the magnetic layer is significantly modified from that of the bulk materials as its thickness is reduced to the order of 10 Å. One of the most important contributions to this change is due to the surface anisotropy energy developed from the interface interaction between the magnetic layer and "non-magnetic" layer which can be expressed as an effective anisotropy energy to the bulk of the magnetic layer such that

$$K_{eff} = K_{sur}/t, \quad (34)$$

where t is the thickness of the magnetic layer. Typical values of the surface anisotropy energy constant, K_{sur} , vary from 0.1 to 1 erg/cm², having a preferred orientation of the magnetization normal to the film. A transition thickness t_{cr} , below which the internal uniaxial anisotropy energy will dominate the magnetostatic anisotropy energy to produce an easy axis normal to the film, exists when the values of the magnetic layer thickness varied from 2 to 10 monolayers in most of the systems. The origin of the surface anisotropy energy may come from the Néel surface anisotropy energy⁴⁶, the magnetostriction energy, the interlayer diffusion or the polarization of the "non-magnetic" surface atoms.

(2) One of the most important contributions of the CFFR technique to the understanding of the magnetic properties of multilayer systems is the evolution of the interlayer exchange constant, A_{12} . For Pt and Pd interlayers, the coupling coefficient is positive producing parallel alignment of the magnetization of the layers. The coupling strength decreases with the increase of the "non-magnetic" layer thickness t_{NM} following roughly an exponential form

$$A_{12} = A_{12}^0 \exp(-t_{NM}/t_0), \quad (35)$$

for which the decay length t_0 is on the order of 10 Å and A_{12}^0 is on the order of 1 to 50 erg/cm², about an order of magnitude smaller than the direct exchange interactions within the magnetic layers.

For Cr, Cu and Ru interlayers, the coupling coefficient oscillates from positive (parallel coupling) to negative (anti-parallel coupling) while the amplitude of the

oscillation decreases as a function of the thickness. The oscillation period was observed to be on the order of 10 Å to 15 Å.

The variation of the exchange interaction through "non-magnetic" layers is similar to the polarization of the host material by the nearby 3d-transition magnetic atoms in a dilute transition metal alloy system. The bare magnetic moment of the dissolved 3d-atom in this system, polarizes its surroundings, and the polarization, as a function of the distance, is governed by the generalized magnetic susceptibility of the host material. If the host material were a normal metal in which the conduction electrons can be treated as free electrons, like in Cu and Ag, this susceptibility $\chi(r)$ will oscillate from positive to negative following the RKKY formula⁴⁷. However if the intra-atomic exchange interactions between the band electrons in the host metal are important, like in Pt and Pd, the susceptibility will differ from the RKKY form and roughly follows an exponential decay form.⁴⁸

$$\chi(r) \propto \frac{1}{r} \exp(-r/r_0). \quad (36)$$

This might explain the fact that no oscillation were found in the Pt and Pd included multilayer systems although the mechanism of the interaction through "pin-holes" in the Pt or Pd layers, is another possibility. The oscillations in the exchange interaction, A_{12} , observed in noble metal interlayers, suggest that a RKKY type interaction plays an important role in the multilayer exchange interaction. However the oscillation period in the Cu included multilayer system is significantly larger than that predicted from the layered RKKY calculation⁴⁴. There is no well known mechanism that accounts for the observed behavior of the coupling mechanism for this structure though a surface roughness model⁴⁹ was proposed to explain the long period oscillations to some extent. In Cr and Ru, the conduction electrons band structures are more complicated than that in the noble metal. They can not be treated using the free electron model. A successful theory must include the details of the band structures near the Fermi surfaces in these "non-magnetic" layers⁵⁰.

As more combinations of coupled magnetic/"non-magnetic" structures are developed and investigated, it is likely that additional new effects will be observed as well as a class of materials having a wider range of variables than those observed to date. It is expected that such structure; will have a variety of useful applications that depend on microstructural properties. At present two such applications include magneto-optical storage media and magnetic readheads for computers.

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